Turbulent Flows

Stephen B. Pope Cambridge University Press (2000)

Solution to Exercise 10.5

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Date: 04/16/03

a:) According to the $k-\varepsilon$ model, the specification of turbulent viscosity is

$$\nu_T = C_\mu k^2 / \varepsilon. \tag{1}$$

So in a simple turbulent shear flow, the shear stress is given by

$$|\langle uv \rangle| = \nu_T \frac{\partial \langle U \rangle}{\partial y} = \nu_T \mathcal{S}.$$
 (2)

Substituting Eq. 1 into Eq. 2, we get

$$\frac{|\langle uv\rangle|}{k} = C_{\mu} \frac{\mathcal{S}k}{\varepsilon}.$$
(3)

For simple turbulent shear flow, the production is

$$\mathcal{P} = |\langle uv \rangle| \frac{\partial U}{\partial y} = |\langle uv \rangle| \mathcal{S}.$$
(4)

Substituting Eq. 3 into Eq. 4, we get

$$\mathcal{P} = C_{\mu} \frac{\mathcal{S}k^2}{\varepsilon} \mathcal{S} = C_{\mu} \frac{\mathcal{S}^2 k^2}{\varepsilon},\tag{5}$$

i.e.,

$$\frac{\mathcal{P}}{\varepsilon} = C_{\mu} \left(\frac{\mathcal{S}k}{\varepsilon}\right)^2 \tag{6}$$

From Eq. 6, we get

$$\frac{Sk}{\varepsilon} = \left(\frac{\mathcal{P}}{C_{\mu}\varepsilon}\right)^{1/2}.$$
(7)

Substituting Eq. 7 into Eq. 3, we get

$$\frac{|\langle uv\rangle|}{k} = C_{\mu}^{1/2} \left(\frac{\mathcal{P}}{\varepsilon}\right)^{1/2},\tag{8}$$

and hence Eq.(10.48) is verified.

b:) The Cauchy-Schwartz inequality (Eq.(3.100)) is

$$-1 \le \rho_{12} \le 1,$$
 (9)

i.e.,

$$\left|\frac{\langle uv\rangle}{\langle u^2\rangle^{1/2}\langle v^2\rangle^{1/2}}\right| \le 1.$$
(10)

Substituting Eq. 3 into Eq. 10, we get

$$C_{\mu} \frac{k^2 \mathcal{S}}{\varepsilon} \le \langle u^2 \rangle^{1/2} \langle v^2 \rangle^{1/2}, \qquad (11)$$

i.e.,

$$C_{\mu} \leq \frac{\langle u^2 \rangle^{1/2} \langle v^2 \rangle^{1/2}}{k} \frac{1}{\mathcal{S}k/\varepsilon}.$$
 (12)

For simple shear flow, the $k - \varepsilon$ model yields for the normal stresses $\langle u^2 \rangle = \langle v_2 \rangle = \langle w^2 \rangle = \frac{2}{3}k$. Thus we obtain

$$C_{\mu} \leq = \frac{2/3}{\mathcal{S}k/\varepsilon}.$$
(13)

c:) For a general flow, according to the turbulent viscosity hypothesis, turbulent production \mathcal{P} is equal to

$$\mathcal{P} = \nu_T \mathcal{S}^2, \tag{14}$$

where \mathcal{S} is the characteristic mean rate of strain (see Eq. 5.143 and see page 131 for the definition of \mathcal{S}). And furthermore, according to the specification of $\nu_T = C_{\mu} k^2 / \varepsilon$ in the $k - \varepsilon$ model, \mathcal{P} is given by

$$\mathcal{P} = C_{\mu} \varepsilon \left(\frac{\mathcal{S}k}{\varepsilon}\right)^2,\tag{15}$$

i.e.

$$\frac{\mathcal{P}}{\varepsilon} = C_{\mu} \left(\frac{\mathcal{S}k}{\varepsilon}\right)^2.$$
(16)

So Eq.(10.50) also holds for a general flow.

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